



# An efficient Wave Based Method for solving Helmholtz problems in three-dimensional bounded domains

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Introduction

WBM

Numerical validation

Conclusions

- 1 Introduction
- 2 The Wave Based Method
- 3 Numerical validation of the WBM for 3D acoustics
- 4 Conclusions



- 1 **Introduction**
  - Vibro-acoustic interactions
  - Numerical modelling approaches for mid-frequency vibro-acoustic problems
- 2 The Wave Based Method
- 3 Numerical validation of the WBM for 3D acoustics
- 4 Conclusions

Introduction

Vibro-acoustics

Numerical modelling

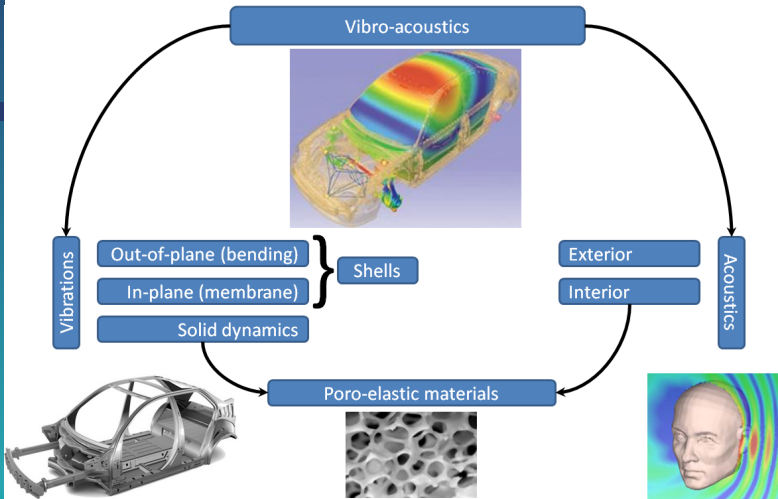
WBM

Numerical validation

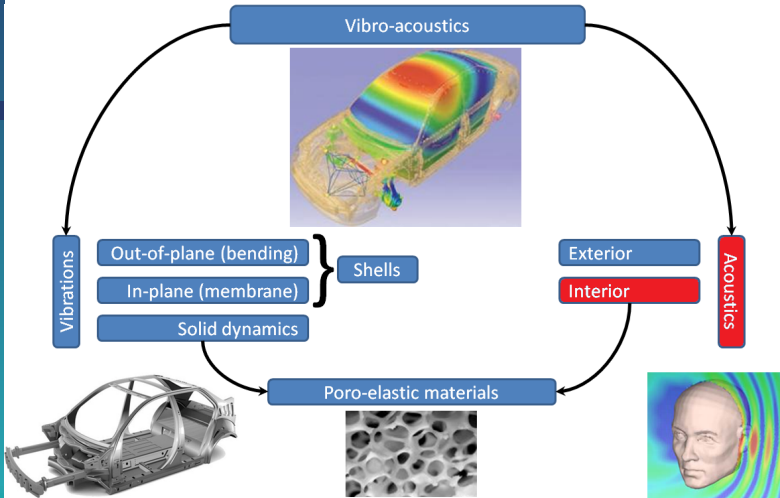
Conclusions



- Introduction
- Vibro-acoustics
- Numerical modelling
- WBM
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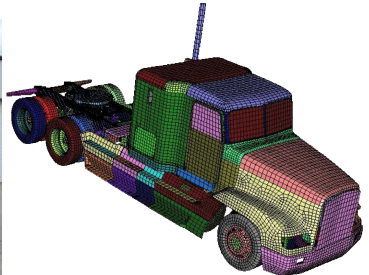
# Simulation of vibro-acoustic systems

Available approaches

*Deterministic element based methods: FEM, BEM,...*

- approximating shape functions
- fine discretisations

⇒ low-frequency



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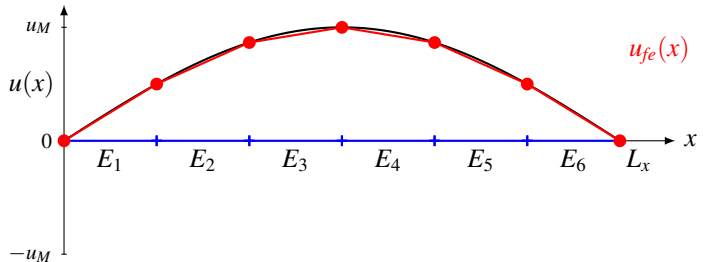
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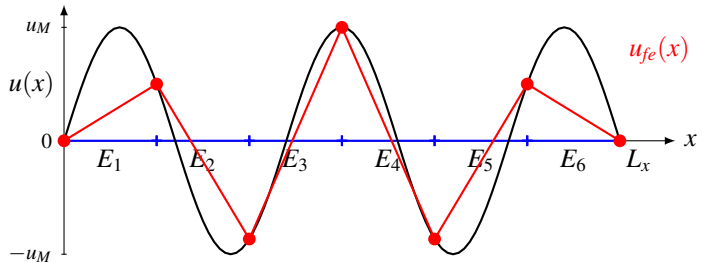
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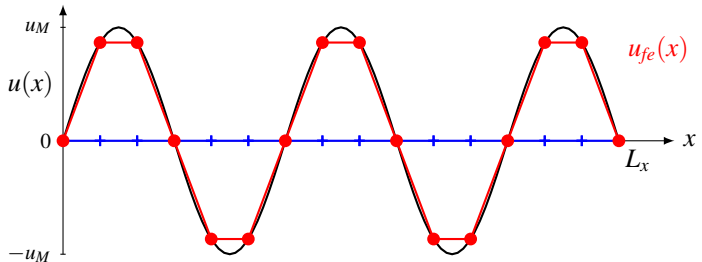
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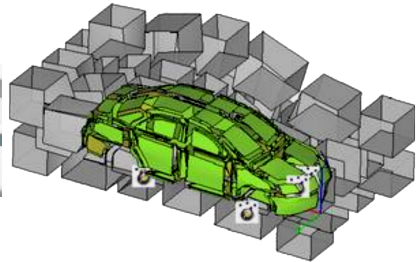
⇒ low-frequency



## *Statistical energy based methods: SEA, EFEM,...*

- energy in SEA subsystems
- underlying assumptions

⇒ high-frequency

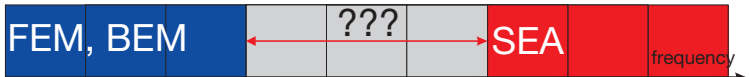


## *Deterministic element based methods: FEM, BEM,...*

- approximating shape functions
- fine discretisations ⇒ low-frequency

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## Deterministic element based methods: FEM, BEM,...

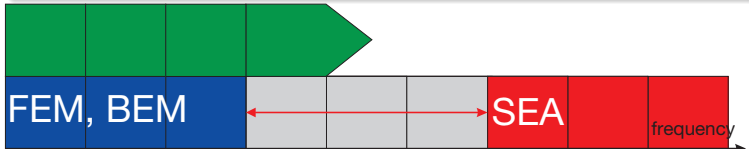
- approximating shape functions
- fine discretisations ⇒ low-frequency

## Statistical energy based methods: SEA, EFEM,...

- energy in SEA subsystems
- underlying assumptions ⇒ high-frequency

## Enhanced deterministic approaches

- Process optimisation
- Reduction or elimination of numerical pollution effects
- Introduction of a priori information (Trefftz approaches)



# Simulation of vibro-acoustic systems

Current research

## *Deterministic element based methods: FEM, BEM,...*

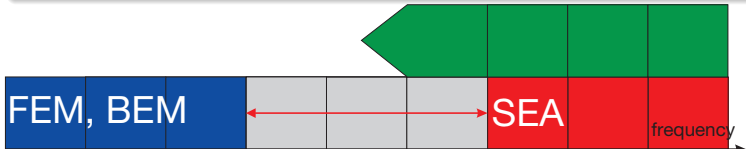
- approximating shape functions
  - fine discretisations
- ⇒ low-frequency

## *Statistical energy based methods: SEA, EFEM,...*

- energy in SEA subsystems
  - underlying assumptions
- ⇒ high-frequency

## *Enhanced statistical approaches*

- Non-equipartition of modal energy
- Strong or indirect coupling
- SEA model parameter estimation



# Simulation of vibro-acoustic systems

Current research

## *Deterministic element based methods: FEM, BEM,...*

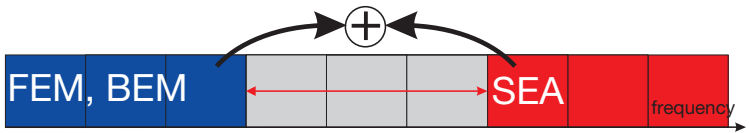
- approximating shape functions
- fine discretisations  $\Rightarrow$  low-frequency

## *Statistical energy based methods: SEA, EFEM,...*

- energy in SEA subsystems
- underlying assumptions  $\Rightarrow$  high-frequency

## *Hybrid deterministic-statistical approaches*

- "Flexible" components: SEA subsystems
- "Stiff" components: FEM models
- Diffuse field reciprocity relation



## *Deterministic element based methods: FEM, BEM,...*

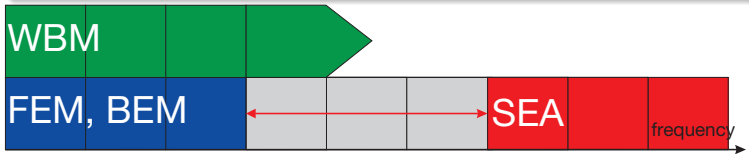
- approximating shape functions
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## *Statistical energy based methods: SEA, EFEM,...*

- energy in SEA subsystems
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## *Deterministic Trefftz-based Wave Based Method*

- Basis functions = exact solutions of governing equations
  - Enhanced numerical convergence properties
- ⇒ applicable to mid-frequency problems



Introduction

**WBM**

Problem definition

WBM concepts

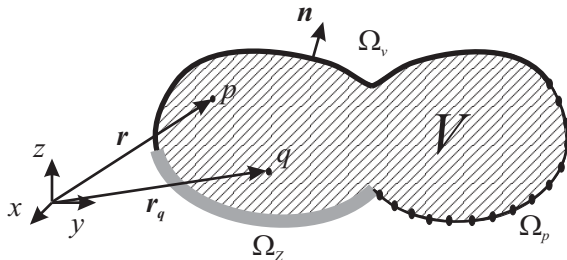
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- 2 **The Wave Based Method**
  - Problem definition
  - Wave Based modelling approach
- 3 Numerical validation of the WBM for 3D acoustics
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- Steady-state dynamic acoustic pressure  $p(\mathbf{r})$  in  $V$ : Helmholtz equation

$$\nabla^2 p(\mathbf{r}) + k^2 p(\mathbf{r}) = \mathcal{F}(\mathbf{r}), \mathbf{r} \in \Omega$$

- At each point of  $\Omega_\bullet$ : 1 boundary condition

$$\begin{cases} \mathbf{r} \in \Omega_v : \mathcal{L}_v(p(\mathbf{r})) = \bar{v}_n(\mathbf{r}), \\ \mathbf{r} \in \Omega_z : \mathcal{L}_v(p(\mathbf{r})) = p(\mathbf{r})/\bar{Z}_n(\mathbf{r}), \\ \mathbf{r} \in \Omega_p : p(\mathbf{r}) = \bar{p}(\mathbf{r}). \end{cases}$$

- 1 Approximation of the field variables within each of the subdomains using physically meaningful **wave functions** en **source terms**

## WBM approximation

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_w p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$

- 1 Approximation of the field variables within each of the subdomains using physically meaningful **wave functions** en **source terms**
- 2 Minimisation of the approximation errors using a Galerkin weighted residual formulation

$$\int_{\Omega_v} \tilde{p}(\mathbf{r}) R_v(\mathbf{r}) d\Omega + \int_{\Omega_z} \tilde{p}(\mathbf{r}) R_z(\mathbf{r}) d\Omega + \int_{\Omega_p} -\mathcal{L}_v(\tilde{p}(\mathbf{r})) R_p(\mathbf{r}) d\Omega = 0$$

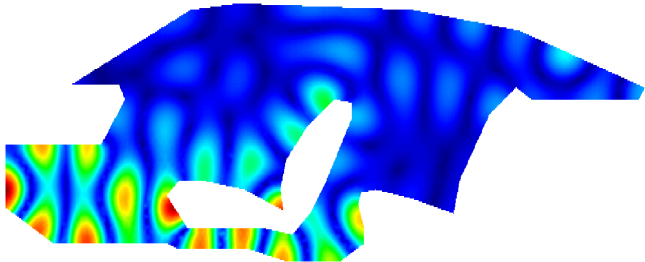


- 1 Approximation of the field variables within each of the subdomains using physically meaningful **wave functions** en **source terms**
- 2 Minimisation of the approximation errors using a Galerkin weighted residual formulation
- 3 Solution of the resulting system of equations

$$\begin{bmatrix} A_w^1 & \dots & C_w^{1,N_\Omega} \\ \vdots & \ddots & \vdots \\ C_w^{N_\Omega,1} & \dots & A_w^{N_\Omega} \end{bmatrix} \begin{Bmatrix} p_w^1 \\ \vdots \\ p_w^{N_\Omega} \end{Bmatrix} = \begin{Bmatrix} F_w^1 \\ \vdots \\ F_w^{N_\Omega} \end{Bmatrix}$$



- 1 Approximation of the field variables within each of the subdomains using physically meaningful **wave functions** en **source terms**
- 2 Minimisation of the approximation errors using a Galerkin weighted residual formulation
- 3 Solution of the resulting system of equations
- 4 Postprocessing, visualisation and interpretation of the response fields



The WB modelling approach has been successfully applied to

## 2D steady-state acoustic analysis

- multi-domain interior acoustics
- acoustic scattering problems
- multiple scattering and inclusion problems

## 2D steady-state structural dynamic analysis

- plate membrane problems
- plate bending problems
- shell analysis

## 2D steady-state vibro-acoustic analysis

- interior vibro-acoustics
- exterior vibro-acoustics

## Current extension:

- 3D steady-state interior acoustics

## Acoustic pressure expansion: bounded subdomains

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_{w=1}^{n_w^{(\alpha)}} p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$

$\Phi_w^{(\alpha)}(\mathbf{r}(x, y, z))$ : *Homogeneous* solutions of Helmholtz eq.

$$\Phi_w(\mathbf{r}(x, y, z)) = \begin{cases} \Phi_{w_r}(x, y, z) = \cos(k_{xw_r}x) \cos(k_{yw_r}y) e^{-jk_{zw_r}z} \\ \Phi_{w_s}(x, y, z) = \cos(k_{xw_s}x) e^{-jk_{yw_s}y} \cos(k_{zw_s}z) \\ \Phi_{w_t}(x, y, z) = e^{-jk_{xw_t}x} \cos(k_{yw_t}y) \cos(k_{zw_t}z) \end{cases}$$

Trefftz approach: the wave number components should satisfy the associated dispersion relation:

$$\begin{cases} (k_{xw_r})^2 + (k_{yw_r})^2 + (k_{zw_r})^2 = \\ (k_{xw_s})^2 + (k_{yw_s})^2 + (k_{zw_s})^2 = \\ (k_{xw_t})^2 + (k_{yw_t})^2 + (k_{zw_t})^2 = k^2 \end{cases}$$



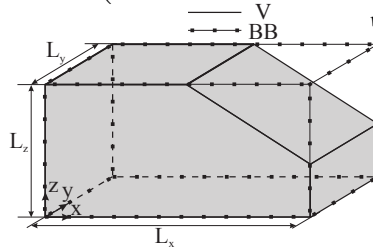
## Acoustic pressure expansion: bounded subdomains

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_{w=1}^{n_w^{(\alpha)}} p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$

$\infty$  number of solutions  $\rightarrow$  selection of wave numbers:

$$\left\{ \begin{aligned} (k_{xw_r}, k_{yw_r}, k_{zw_r}) &= \left( \frac{w_1\pi}{L_x}, \frac{w_2\pi}{L_y}, \pm\sqrt{k^2 - (k_{xw_r})^2 - (k_{yw_r})^2} \right) \\ (k_{xw_s}, k_{yw_s}, k_{zw_s}) &= \left( \frac{w_3\pi}{L_x}, \pm\sqrt{k^2 - (k_{xw_s})^2 - (k_{zw_s})^2}, \frac{w_4\pi}{L_z} \right) \\ (k_{xw_t}, k_{yw_t}, k_{zw_t}) &= \left( \pm\sqrt{k^2 - (k_{yw_t})^2 - (k_{zw_t})^2}, \frac{w_5\pi}{L_y}, \frac{w_6\pi}{L_z} \right) \end{aligned} \right.$$

$$w_1, \dots, w_6 = 0, 1, \dots$$





## WBM approximations: wave functions

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_w p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$

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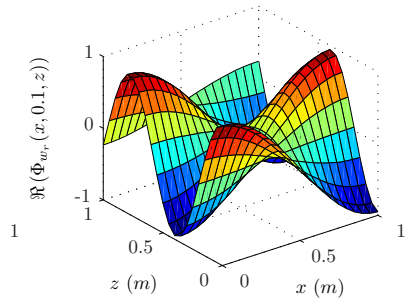
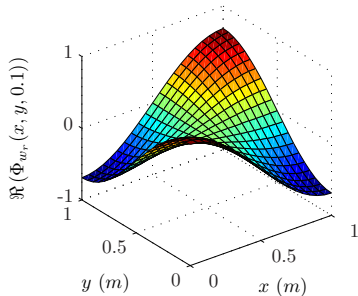
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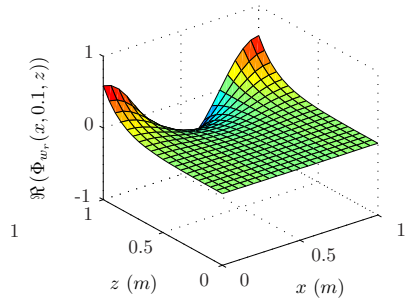
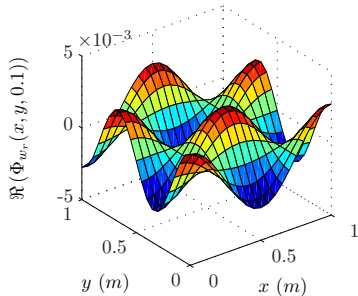
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## Acoustic pressure expansion: bounded subdomains

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_{w=1}^{n_w^{(\alpha)}} p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$

$\hat{p}_q^{(\alpha)}(x, y, z)$ : *Particular* (free field) solution of Helmholtz eq.

- Acoustic point source:

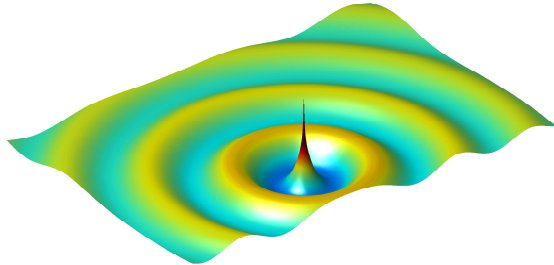
$$\hat{p}_q(x, y, z) = \frac{j\rho_0\omega Q}{4\pi} \frac{e^{-jkr_q}}{r_q}$$

with  $Q$  the source strength  $Q = \int_V q \, dV$  and with  $r_q$  the distance to the source point.



## WBM approximation: source terms

$$p^{(\alpha)}(\mathbf{r}) \simeq \sum_w p_w^{(\alpha)} \Phi_w^{(\alpha)}(\mathbf{r}) + \hat{p}_q^{(\alpha)}(\mathbf{r})$$



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Application of a Galerkin weighted residual formulation yields

$$\begin{bmatrix} A_w^1 & \cdots & C_w^{1,N\Omega} \\ \vdots & \ddots & \vdots \\ C_w^{N\Omega,1} & \cdots & A_w^{N\Omega} \end{bmatrix} \begin{Bmatrix} p_w^1 \\ \vdots \\ p_w^{N\Omega} \end{Bmatrix} = \begin{Bmatrix} F_w^1 \\ \vdots \\ F_w^{N\Omega} \end{Bmatrix}$$

Properties:

- + Small number of degrees of freedom
  - + No accuracy decrease for derived variables
  - + High convergence rate
  
  - Fully populated matrices with complex coefficients
  - Frequency-dependent matrices
  - More complex numerical integrations
  - Bad numerical conditioning
  - Convergence only guaranteed for convex (sub)domains
- applicable to practical mid-frequency applications of moderate geometrical complexity

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Spatial results

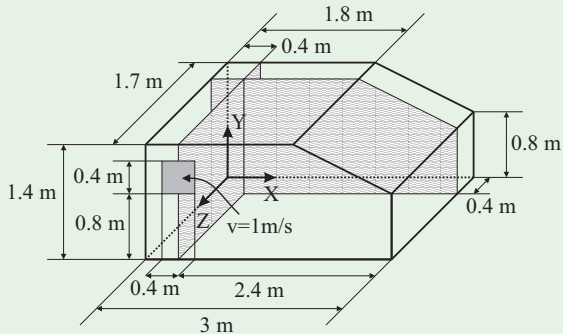
Efficiency

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  - Problem setting
  - Spatial predictions of acoustic quantities
  - Computational efficiency comparison
- 4 Conclusions



## Problem definition



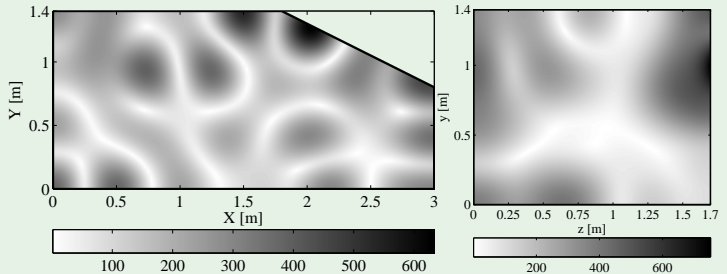
- Acoustic fluid: Air

$$c = 340\sqrt{1 + j\eta} \text{ m/s}, \rho_0 = 1.225/(1 + j\eta) \text{ kg/m}^3, \eta = \{0\%.1\%\}$$

- Boundary conditions: acoustically rigid ( $\bar{v}_n(\mathbf{r}) = 0$ )
- Excitation: discontinuous unit normal velocity on patch in front

## Acoustic variables at 450Hz, damped case

- Acoustic pressure amplitude [Pa]



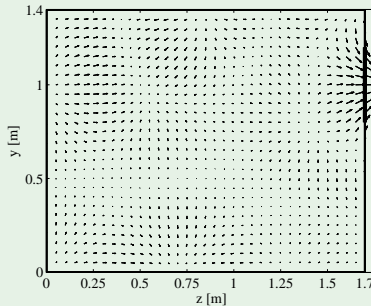
Rigidity conditions accurately taken into account





## Acoustic variables at 450Hz, damped case

- Acoustic velocity vector field [m/s]

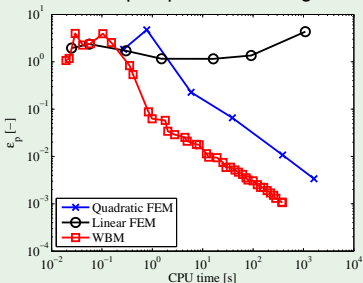


Discontinuous velocity excitation conditions accurately taken into account

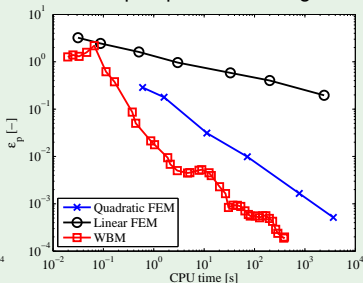


## Computational efficiency comparison at 450Hz

Undamped problem setting



Damped problem setting



$$\epsilon_p = \frac{1}{108} \sum_{j=1}^{108} \epsilon_j = \frac{1}{108} \sum_{j=1}^{108} \left| \frac{\hat{p}(\mathbf{r}_j) - p_{ref}(\mathbf{r}_j)}{p_{ref}(\mathbf{r}_j)} \right|$$

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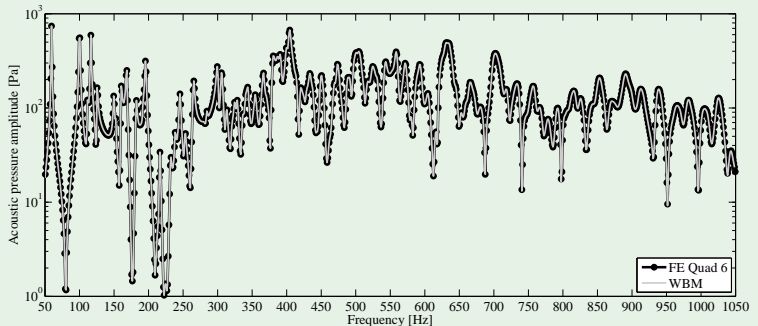
Spatial results

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## Frequency response comparison damped problem setting



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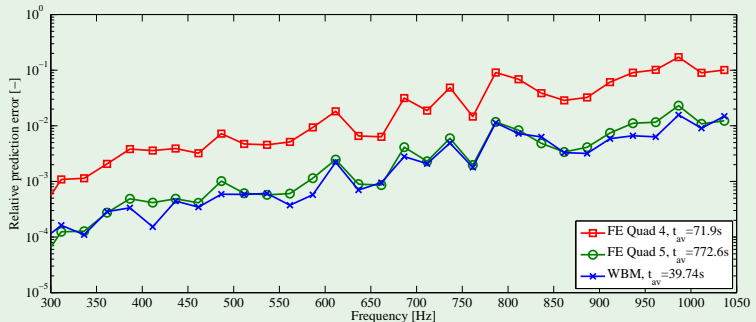
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Relative pressure amplitude prediction errors  
damped problem setting

- For a similar calculation time, the WBM is an order of magnitude more accurate than the quadratic FEM
- WBM reaches a similar prediction accuracy more than 10 times faster than the quadratic FEM.

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## Wave Based Method for steady-state dynamics

- + globally defined exact solutions = wave functions
- + low, mid (and high) frequency applications

## Extension to 3D acoustics

- Derivation of wave function sets
  - Weighted residual formulation
- ⇒ Efficient modelling of 3D problems of moderate geometrical complexity



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## Next steps

Extension of the modelling approach to:

- 3D multi-domain acoustic problems
- 3D acoustic (multiple) scattering problems
- 3D acoustic multiple inclusion problems

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# Thank you for your attention!

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